

the Energy to Lead

CSA NGV4.3 Temperature Compensation and Full Fills-

NGV Technology Forum

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Gas Technology Institute

ESTABLISHED 1941

Gas Technology Institute Overview

Natural Gas Research and Development Focus

- > Staff of 300+
- > 350 active projects
- > 1,200 patents; 500 products



List of Topics

- > Recently Published CSA NGV4.3 Standard
 - Coverage
 - Usefulness
 - Next Phase
- > Discuss temperature compensation
- > Barriers/solutions to better vehicle fills – CEC/SoCalGas Project
 - Controls/Algorithms
 - Gas Conditioning
 - Communications

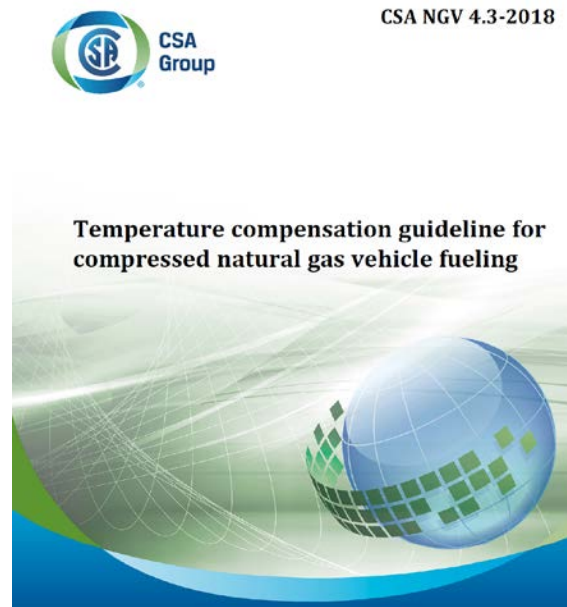


New CSA NGV4.3 Standard

SOME THINGS
ARE EASY....



SOME THINGS
ARE NOT....



CSA NGV 4.3 IS NOW PUBLISHED!

CSA NGV4.3-2018 - Temperature Compensation Guideline

> What it is:

- Safety performance **guideline** to prevent dispensing systems from exceeding a safe fill level into NGV storage
- Used for assessing proper temperature compensation of **in-service** commercial dispensing systems
- Informs on natural **gas composition** variability impact

> What it is not:

- Not a **listing standard** to certify newly manufactured dispensers or fueling appliances
- Not a methodology on “**how**” to temperature compensate
- Not intended to constrain innovation or technology

CSA NGV4.3-2018 - Content

- > Background – Theory
- > Temperature/Pressure Tables
 - Relationships away from Standard conditions of 3,600psig & 70F (24.82 MPa & 21C)
 - Safe limits for gas composition extremes
- > Test Equipment & Methods
- > Test Conditions
- > Informative Annex



CSA NGV4.3 Figures

Table 1
Gas temperature/settled pressure relationships — P36 service pressure
 (See Clauses 5.1, 5.3, 5.5, 6.2, and 6.4.)

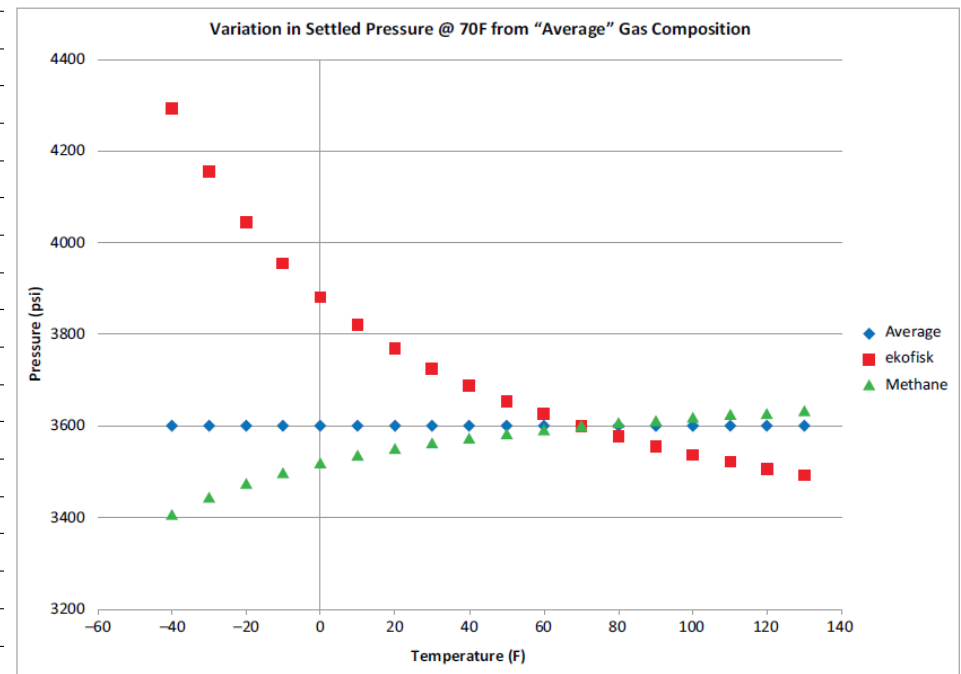
Temperature °F (°C)	Pressure psi (kPa)	Pressure psi (kPa)
	Nominal Gas Composition	Conservative Gas Composition
130 (54)	4,500 (31 026)*	4,500 (31 026)*
120 (49)	4,437 (30 592)	4,395 (30 302)
110 (43)	4,270 (29 441)	4,237 (29 213)
100 (38)	4,103 (28 289)	4,078 (28 117)
90 (32)	3,935 (27 131)	3,919 (27 021)
80 (27)	3,768 (25 979)	3,759 (25 917)
70 (21)	3,600 (24 821)†	3,600 (24 821)†
60 (16)	3,432 (23 663)	3,409 (23 504)
50 (10)	3,264 (22 504)	3,218 (22 187)
40 (4)	3,096 (22 346)	3,027 (20 870)
30 (-1)	2,928 (20 188)	2,836 (19 554)
20 (-7)	2,760 (19 030)	2,646 (18 244)
10 (-12)	2,592 (17 871)	2,455 (16 927)
0 (-18)	2,424 (16 713)	2,266 (15 624)
-10 (-23)	2,256 (15 555)	2,077 (14 320)
-20 (-29)	2,089 (14 403)	1,888 (13 017)
-30 (-34)	1,922 (13 252)	1,701 (11 728)
-40 (-40)	1,755 (12 100)	1,515 (10 446)

Note: The maximum temperature of the vehicle container shall not exceed 85 °C (185 °F) per CSA NGV 2.

* Maximum allowable fill pressure regardless of ambient temperature.

† Service pressure 24.82 MPa (3,600 psi) at 21 °C (70 °F).

Figure C.2
Variation in settled pressure
 (See Clauses 5.1, 5.3, 6.2, and 6.4.)



CSA NGV4.3-2018 - Practical Use

- > Periodic safety checks by station owner/operators
- > Commissioning into service criteria
- > Baseline performance and trending data
- > Pass/fail criteria for future listing Standards



CSA NGV4.3-2018 - Next Phase

- > Expand scope of NGV4.3 to include test methodology for:
 - New dispenser certification test
 - Residential Fueling Appliances
 - Vehicle Fueling Appliances
- > Standardize on a pressure/temperature test
- > Have all other standards reference NGV4.3 for TC



CNG Full Fill Project

- >CEC, PIR-14-013
- >Cofunding:
 - SoCalGas, UTD, SMP
- >TAC:
 - ANGI, Agility, SoCalGas, NREL
- >Goal:
 - Improve CNG full fills



Project Focus

- > Fill simulation
- > Dispenser algorithms
- > Communication
- > Precooling
- > Testing

Fill Simulation

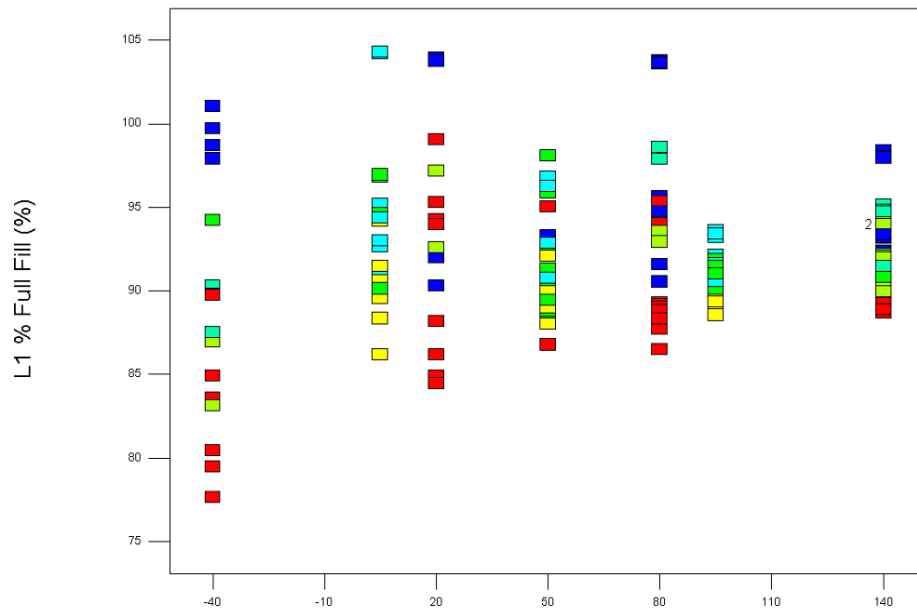
- > Matlab Simulink
- > Uses real gas properties from NIST Refprop
- > Simulates cascade and direct fill scenarios
- > Coupled with design of experiments to run hundreds of cases that vary:
 - Starting pressure
 - Starting temperature
 - Tank size
 - Gas composition
 - Etc.

Dispenser Algorithm

- > Fill algorithm has significant impact on full fill and safety
- > Extremely challenging to develop accurate algorithm
 - Tank temperature, gas composition
- > Often tank pressure limit is reached before full fill
- > Mass algorithm issues
- > Pressure and temperature based algorithm is likely best path forward at this time

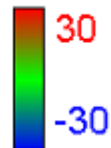
Simulation Example

Algorithm 1

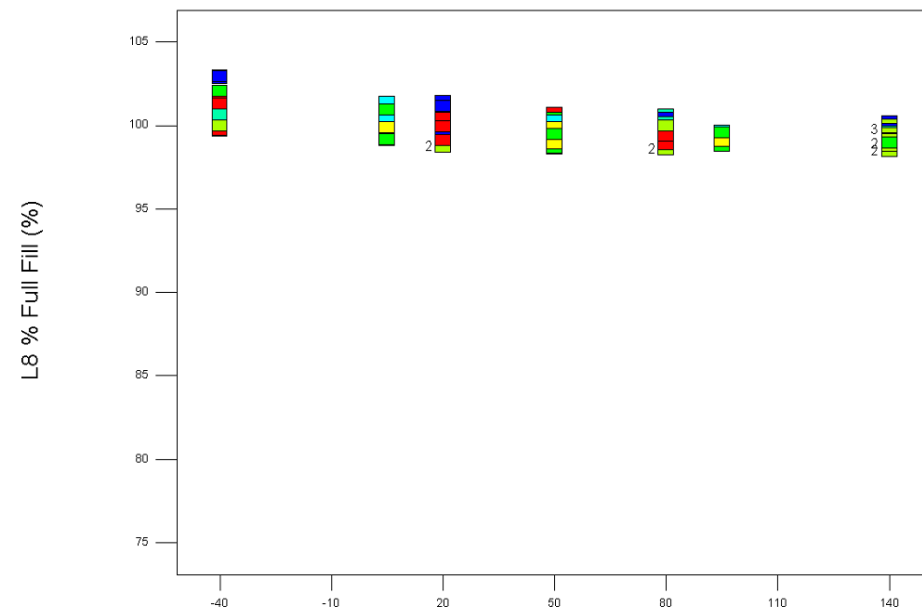


A: Ambient Temp (degF)

B: Vehicle Tank Temp



Algorithm 8



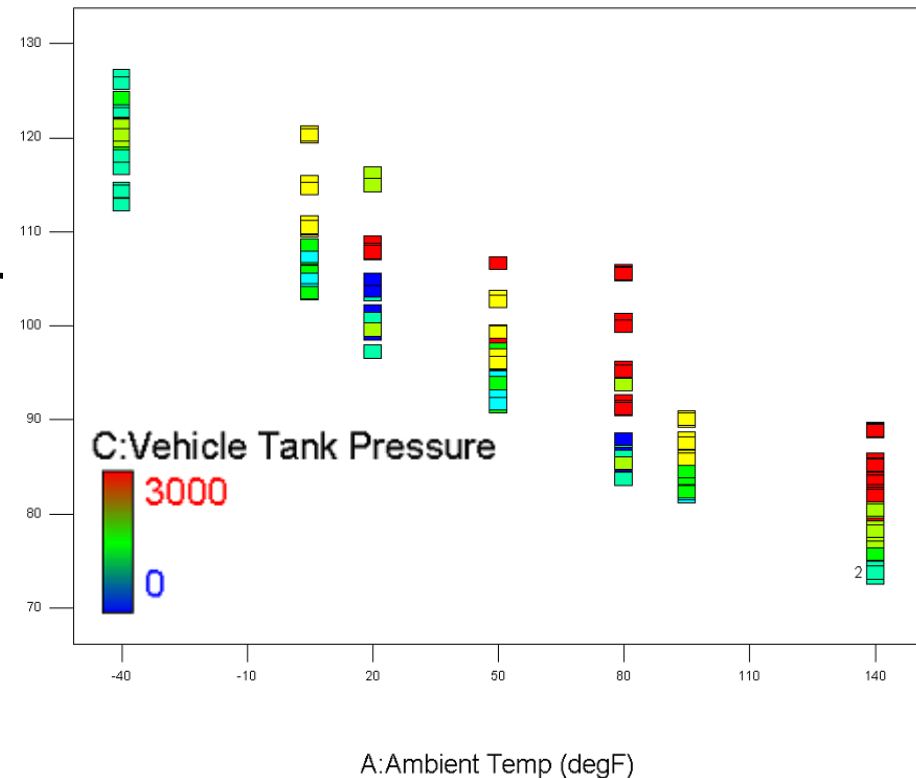
A: Ambient Temp (degF)

Communication

- > CNG industry should consider vehicle/dispenser communication
- > Hydrogen industry requires IR communication
- > IR works, but requires hardware modifications
- > GTI investigating wireless communication protocols
- > Can be used to transmit pressure, temperature, volume, tank type, tank expiration date, etc.
- > Could even track vehicle inspections

Precooling

- > Necessary to achieve full fills above 20-30F
- > Technologies:
 - Traditional chiller
 - Back pressure regulator
 - CNG compressor as chiller
 - Turboexpander
- > Alternatives:
 - Fill/Discharge cycles



Other recommendations

- > Develop standard for CNG communication
 - Commit to communication method
 - Ensure safe, secure and accurate data transmission
- > Develop standard for dispenser algorithm
 - With and without communication
 - Makes dispenser certification easier
 - Moves risk away from manufacturers
 - Improves safety

Thank you!

Backup slides

Dispenser Improvement Opportunities

There are still several aspects of vehicle and dispenser design which could be modified to further improve the fueling experience.

- > Change the tank design and/or modify the code to eliminate the 4500 PSIG restriction
- > Inject cool gas into the cylinder (at temperatures below ambient)
- > Improve algorithms
 - Incorporate validated heat of compression factors that properly account for temperature of injected gas etc.
 - Eliminate calculation errors
 - Reduce instrumentation error
- > Further reduce hydraulic losses in the hose components and on the vehicle

Additional Equipment Improvement Opportunities

- > Select the appropriate dispenser design based upon the fueling application
- > Reduce the hydraulic losses within the dispenser and hose assemblies by utilizing high flow, low pressure drop components; ANGI has standardized on full flow activated ball valves and tubing with a minimum 1" diameter
- > Incorporate the appropriate fueling strategy & algorithm. Percentage of fill before reaching vehicle limitations is affected by the following
 - Initial vehicle tank pressure
 - Tank PRV set point
 - Heat of compression & ambient conditions
 - Hydraulic losses in filling circuit (dispenser & vehicle)

Valve Panels

Compressor

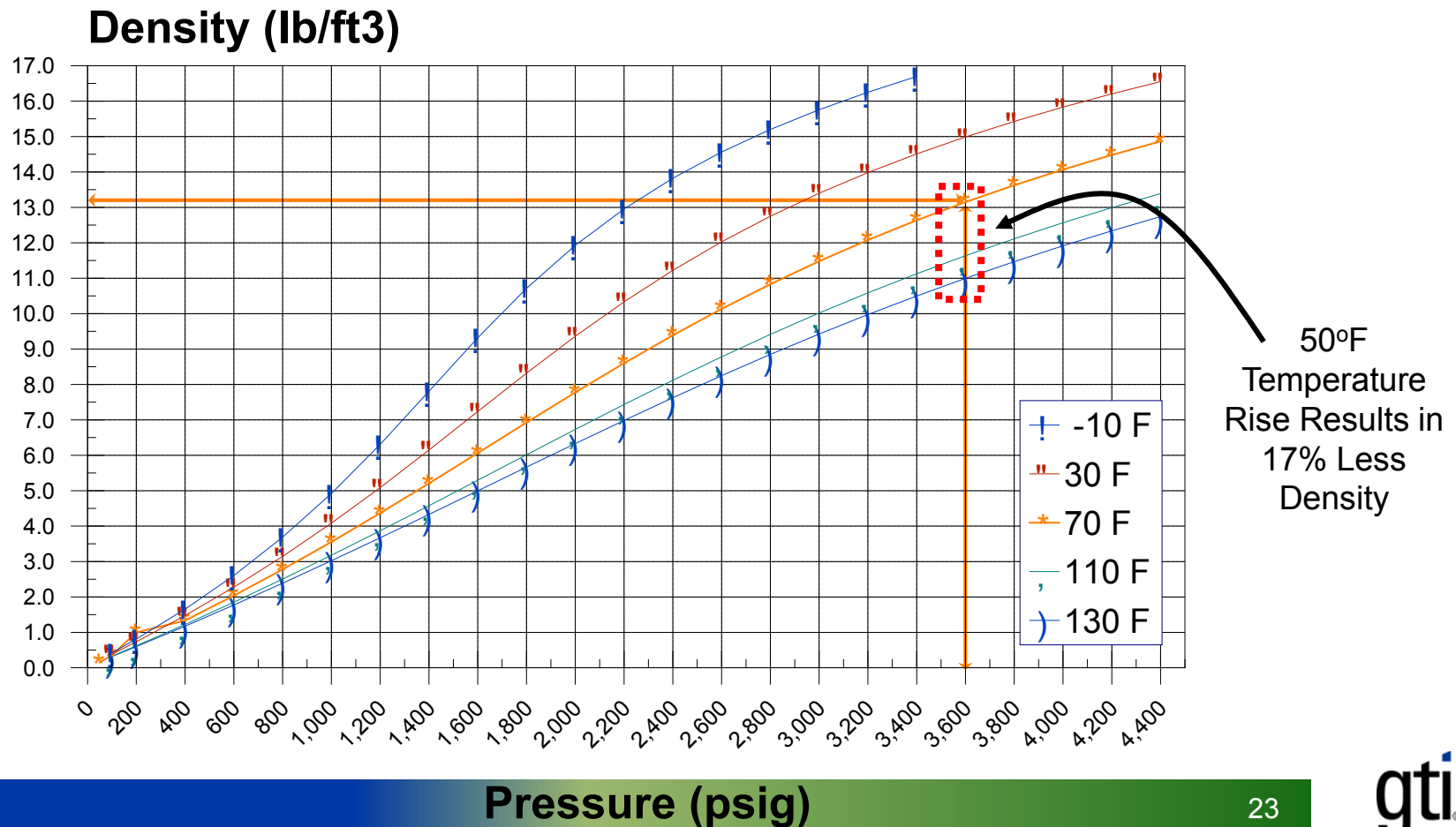
Site & Vehicles

Potential Solutions

- Pre cooling gas before the gas enters the vehicle.
(Expensive and high maintenance)
- Redundant pressure transducers in the dispenser to provide a more precise measurement of the filling process.
- Raising the relief valve pressure in the dispenser to 5000 psi.
- Tank manufactures using realistic numbers and volumetric numbers that account for the limitations of the technology today. (Useable volume)
- Establishing an industry protocol to measure internal tank pressure and temperature when available.

Example: Natural Gas

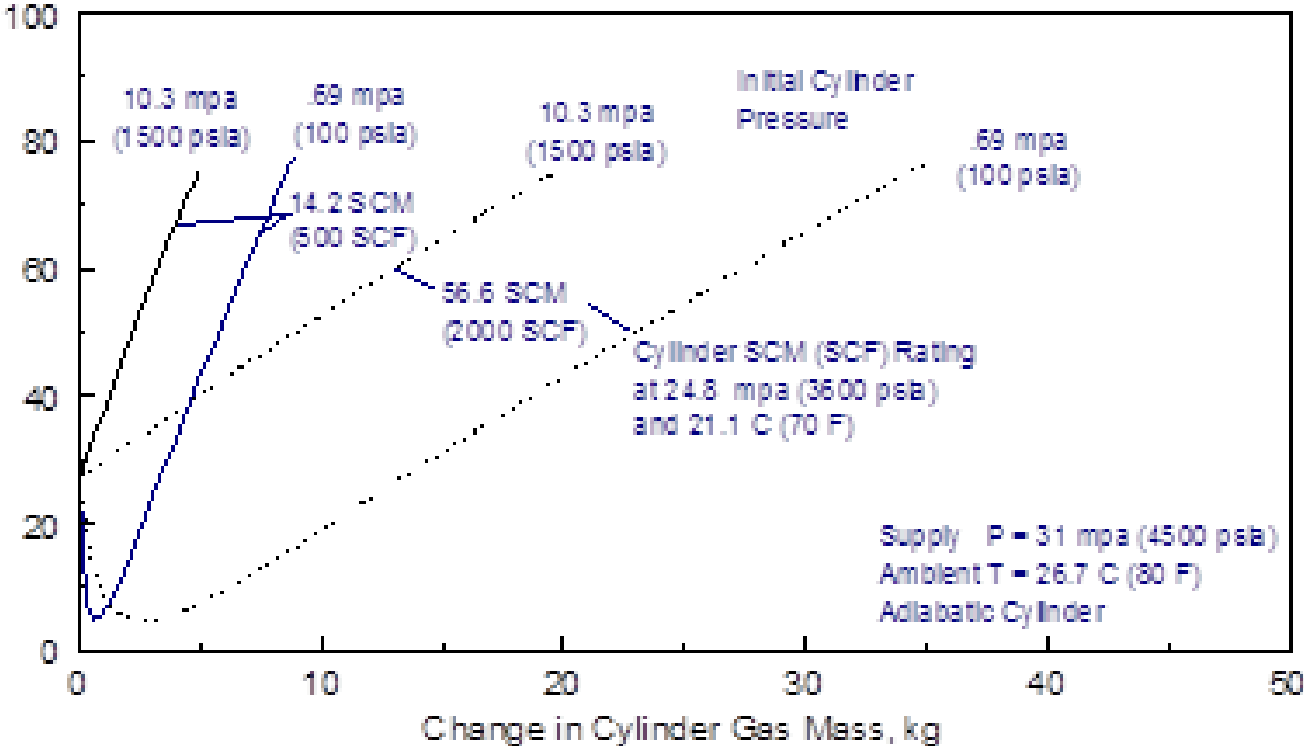
NGV Fuel Storage Characteristics



Example: Natural Gas

Cylinder temperature is a function of the change in injected gas mass, initial pressure, and cylinder volume

Cylinder Temperature, C

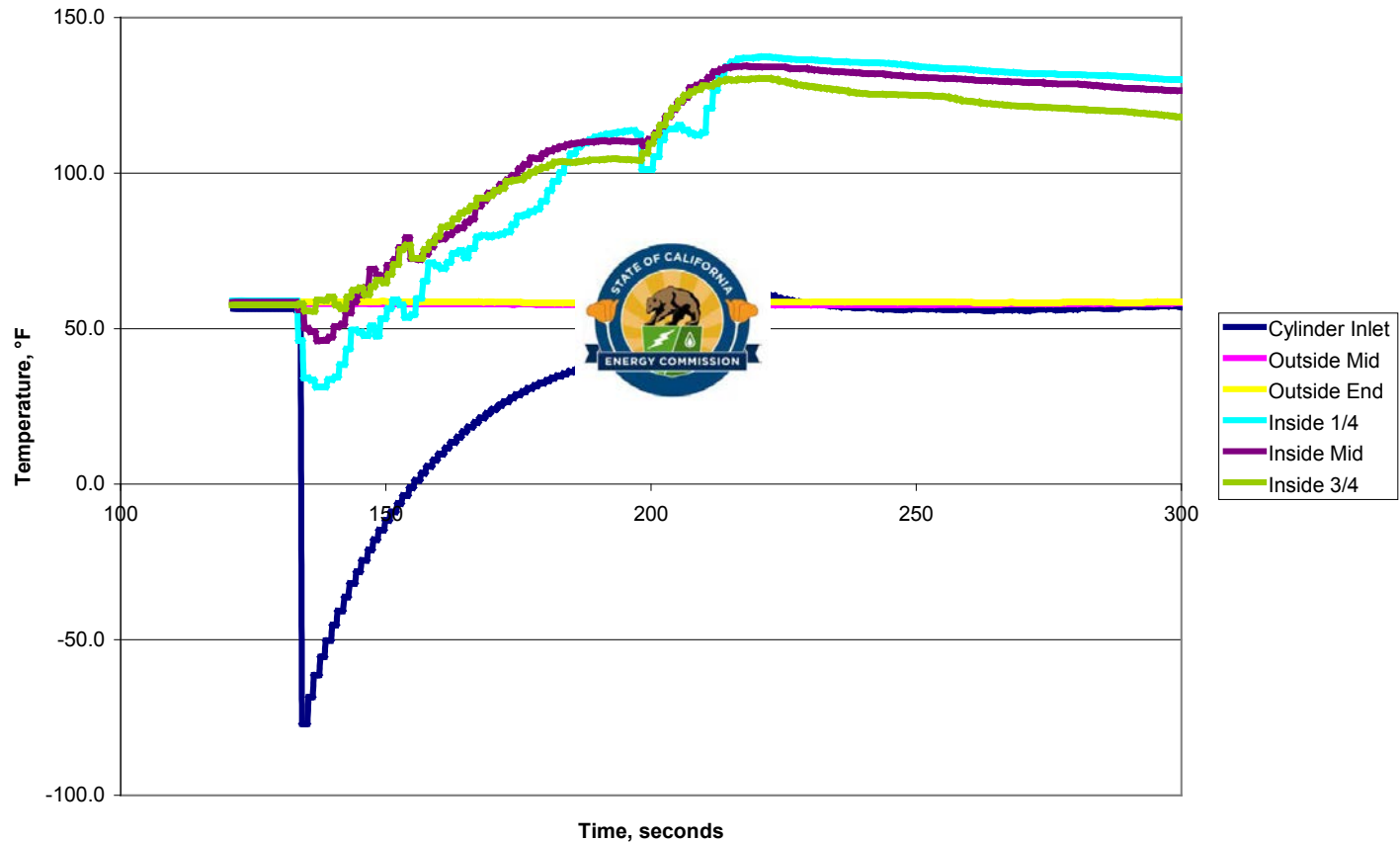


7.8GGE

13.75GGE

When it comes to Temperature....location matters

Example: Type 2 (Steel) – Natural Gas (3000 psig fill pressure)



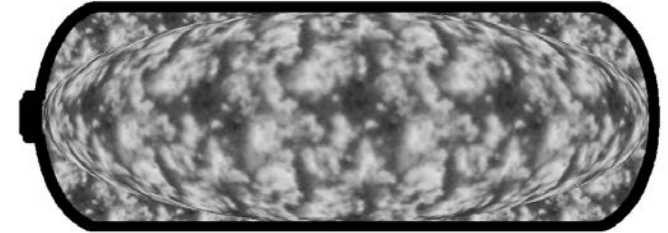
GTI CHARGE Model

- > Modeling Tool
 - Characterizes Dynamic Fast-Fill Process
- > Assess Cylinders of Different Size & Construction
- > Various Starting & Ending Fill Conditions
 - Cylinders
 - Ground Storage
- > Used To Create Dispenser Filling Algorithms

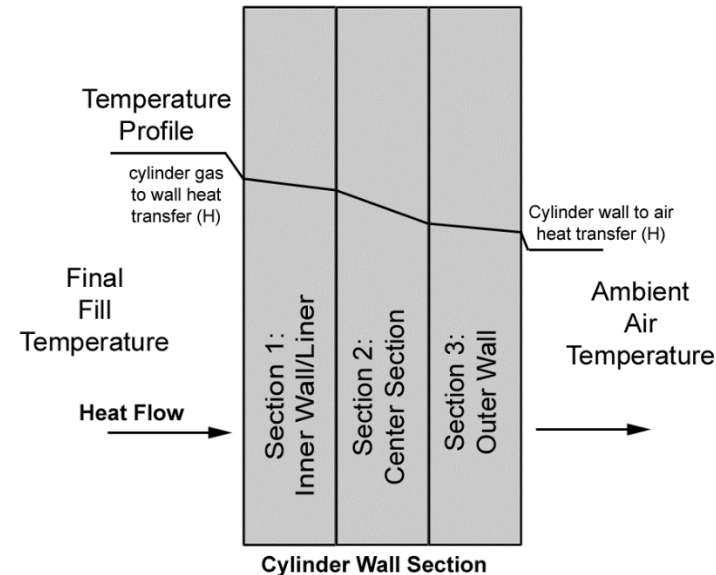
GTI CHARGE Gas Cylinder Filling Model

First Principle Thermodynamic Model

Addresses in-cylinder gas dynamics and heat transfer phenomena



GTI CHARGE MODEL GAS CYLINDER FILLING



Model captures dynamic gas filling effects, gas to cylinder heat transfer, and heat transfer from cylinder to ambient

GTI CNG AccuFill® Algorithm

- > GTI developed & patented technology to address CNG temperature rise during mid-1990s
- > Technology licensed to several worldwide manufacturers, but not integrated
- > Provides more consistent fill performance over wide range of ambient conditions
- > Tech Transfer to Commercial Dispenser(s) Design Needed.

United States Patent [10]	[11] Patent Number: 5,771,948
Kountz et al.	[15] Date of Patent: Jun. 30, 1998

[54] AUTOMATED PROCESS FOR DISPENSING COMPRESSED NATURAL GAS	[57] ABSTRACT
[73] Inventor: Kenneth J. Kountz, Polkate, William E. Liss, Libertyville, Christopher E. Hines, Palos Hills, all of IL	A method and apparatus for dispensing natural gas into the natural gas vehicle cylinder of a motor vehicle is disclosed. The natural gas dispensing system includes a pressure transducer and a temperature transducer for measuring the pressure and temperature, respectively, of the supply gas as it is passed toward a dispenser, a natural pressure transducer for measuring the pressure within the natural gas vehicle cylinder, an ambient air temperature transducer for measuring ambient air temperature at the dispensing site, and a mass flow meter for measuring the gas mass injected into the vehicle cylinder. Each transducer and the mass flow meter sends a data signal to a control processor which automatically dispenses compressed gas to the vehicle cylinder, as well as measuring the amount of gas mass injected into the cylinder. The control processor maintains the mass of compressed gas injected into the vehicle cylinder by injecting a first mass of compressed gas into the cylinder and calculating a first volume estimate in response thereto, estimating a second mass of compressed gas required to fill the cylinder to a first predetermined fill state, and then estimating a third mass of compressed gas required to fill a reference gas cylinder to the first predetermined fill state in response thereto. Thereafter, the second mass of compressed gas is injected into the cylinder, the gas mass being injected into the cylinder from the initial state being measured, as well as the pressure of the compressed gas within the container resulting from the injection of the second gas mass being measured, whereupon the control processor estimates a second volume of the gas container in response thereto. Thereafter, the control process may be used to either perform a final fill step to complete the gas mass injection into the cylinder, or may perform a second intermediate fill step prior to the final fill step for greater accuracy in determining tank volume during the fill process.
[75] Assignor: Gas Research Institute, Chicago, IL	
[21] Appl. No: 878,088	
[22] Filed: Jun. 15, 1997	
Related U.S. Application Data	
[62] Division of Ser. No. 08,970, filed 03, 1996.	
[31] Int. Cl. ⁷	B6H 1/38, B6H 5/20
[32] U.S. Cl.	140/83, 141/2, 141/4, 141/18, 141/39, 141/95, 141/91, 141/197
[38] Field of Search	141/7, A, 38, 39, 141/48, 49, 51, 82, 83, 197, 222/146/6, 731/49, 290 B
References Cited	
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5,406,908	4/1995 Harkin 141/2
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5,911,283	7/1999 Schulz et al. 141/197
Primary Examiner—Billey J. Reilly Assistant Examiner—Timothy L. Mauer Attorney, Agent, or Firm—Thomas, Kayden, Horanowitz & Keefe, L.L.P.	

United States Patent [10]	[11] Patent No.: US 7,059,364 B2
Kountz et al.	[15] Date of Patent: Jun. 13, 2006

[54] CONTROL METHOD FOR HIGH-PRESSURE HYDROGEN VEHICLE FUELING STATION DISPENSERS	[52] U.S. CL.
[75] Inventor: Kenneth John Kountz, Polkate, IL (US); Kenneth Robert Kritha, New Lenoir, IL (US); William E. Liss, Libertyville, IL (US)	141/8; 141/92; 141/93; 141/197
[73] Assignor: Gas Technology Institute, Dan Plains, IL (US)	[58] Field of Classification Search
(*) Notice: Subject to any disclaimer, the term of this patent is extended or adjusted under 35 U.S.C. 154(b) by 0 days.	141/8, 38, 39, 40, 49, 51, 82, 83, 197, 222/146/6
[21] Appl. No: 18911,038	See application file for complete search history.
[22] Filed: Aug. 5, 2004	
[65] Prior Publication Data	
US 2005/017845 A1 Aug. 18, 2005	
Related U.S. Application Data	
[60] Provisional application No. 60/543,895, filed on Feb. 12, 2004.	
[51] Int. Cl. ⁷	
B6H 1/00 (2006.01)	

[56] References Cited	
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6,786,341 B1 *	6/2004 Ischebarger et al. 141/4
* cited by examiner	
Primary Examiner—Timothy L. Mauer [74] Attorney, Agent, or Firm—Mark E. Fejer	
[57] ABSTRACT	
A method for quick filling a vehicle hydrogen storage vessel with hydrogen, the key component of which is an algorithm used to control the fill process, which interacts with the hydrogen dispensing apparatus to determine the vehicle hydrogen storage vessel capacity.	
3 Claims, 9 Drawing Sheets	

Pressure related to fuel composition

> Gas composition impacts temp comp. pressure

> GM chart uses pressure limits for worst case conditions

> Difficulties on mandating max. settled pressures

> Temp comp. vehicle gauge could help

Temperature Compensated Fill Chart

Using two “extreme” Natural Gas available/measured compositions – one cleaner (> 97 mol% CH₄) and the other with ~ 75 mol% CH₄

Temperature (°F)	Pressure (psia)	Density (g/cm ³)	Temperature (°F)	Pressure (psia)	Density (g/cm ³)
130	4558.7	0.197	130	4709.7	0.247
120	4399.4	0.197	120	4525.1	0.247
110	4239.9	0.197	110	4340.4	0.247
100	4080.2	0.197	100	4155.4	0.247
90	3920.2	0.197	90	3970.4	0.247
80	3760.2	0.197	80	3785.3	0.247
70	3600	0.197	70	3600	0.247
60	3439.5	0.197	60	3414.8	0.247
50	3279	0.197	50	3229.6	0.247
40	3118.3	0.197	40	3044.5	0.247
30	2957.6	0.197	30	2859.5	0.247
20	2796.9	0.197	20	2674.8	0.247
10	2636.1	0.197	10	2490.4	0.247
0	2475.3	0.197	0	2306.4	0.247
-10	2314.7	0.197	-10	2122.9	0.247
-20	2154.1	0.197	-20	1940.3	0.247
-30	1993.8	0.197	-30	1758.5	0.247
-40	1833.8	0.197	-40	1577.9	0.247

Conservative approach : maximum allowable fill pressure corresponding to worst case scenario

Temperature (°F)	Pressure (psig)	Temperature (°C)	Pressure (psig)
130	4500*	55	4500*
120	4399	50	4426
110	4240	40	4142
100	4080	30	3857
90	3920	21	3600**
80	3760	10	3230
70	3600**	0	2894
60	3415	-10	2558
50	3230	-20	2222
40	3045	-30	1886
30	2860	-40	1578
20	2675		
10	2490		
0	2306		
-10	2123		
-20	1940		
-30	1759		
-40	1578		

* Maximum allowable fill pressure regardless of ambient temperature
 ** Service pressure 3600 psig (24,800 kPa) at 70 F (21 C)
 To be removed by customer only. 23259015

Defining the Impact

- > Significant under-filling affects major issues in the industry:
 - Cost (up to 10% of conversion cost)
 - Range (100's of miles – 30 GGE “missing” on HD trucks with 150 GGE of storage)
 - Weight/Space (critical for important markets)
 - Fuel economy (impacts environmental, cost, and range concerns)
 - Customer Satisfaction – misunderstandings lead to bad experiences and disappointments

Primary Safety Concern: Temperature Compensation

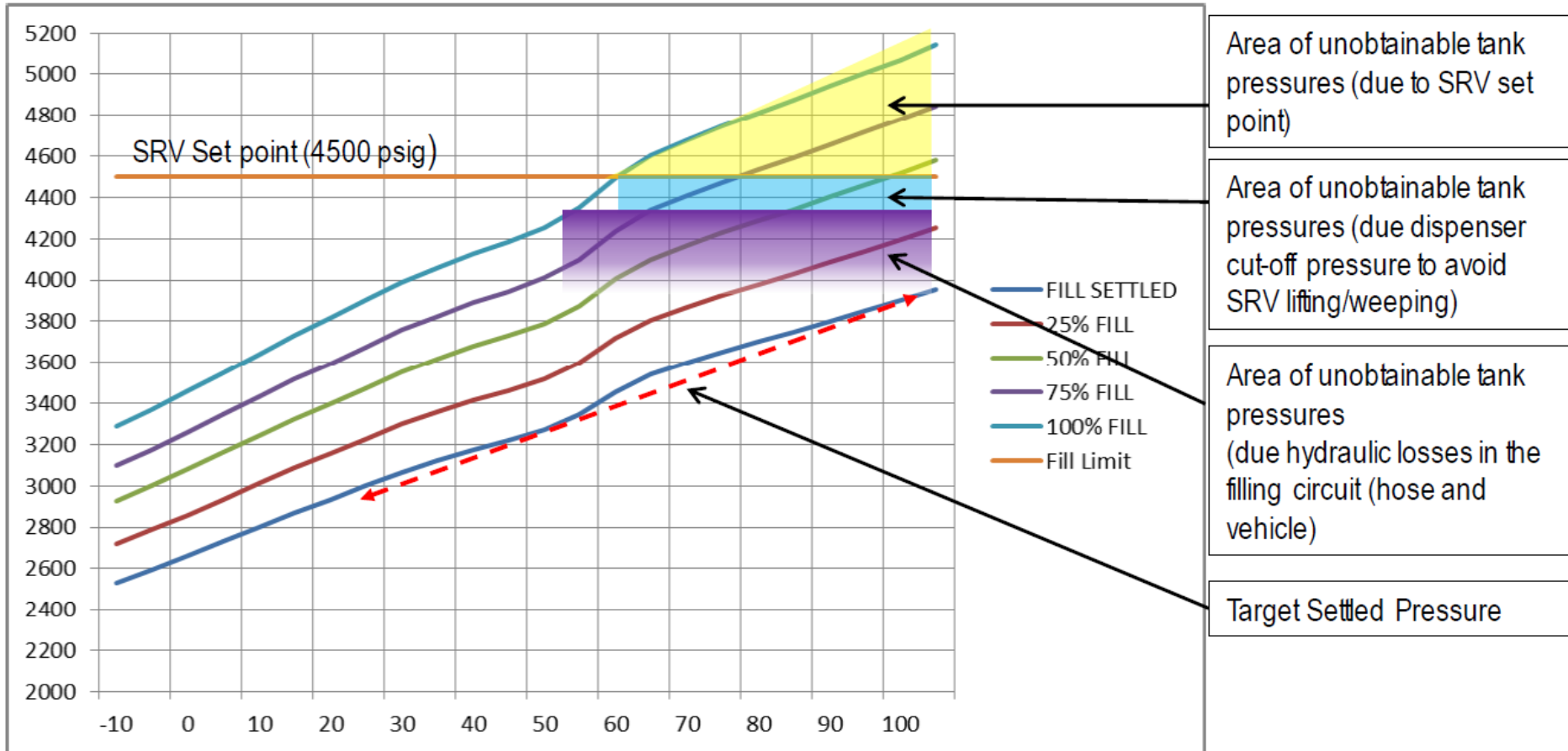
- > Temperature Compensation: For a given gas composition, there is a constant density that equals 3600 psi at 70 °F (~0.21 g/cm³ for typ. NG)
- > Safety is primary concern-dispensers use of temperature compensation is important
 - Without compensation a fill can occur at high pressures in very cold conditions resulting in over-filling
 - CVEF white paper defines issue and best practices
 - Accountability and verification is key
- > CSA NGV 4.3 – Tasked with addressing this issue
 - Initial topic: Defining settled pressure at various temps

Full-Fills: Optimized Temperature Compensation

- > Temperature compensation is also important part of full-fill considerations but only one side of the issue
- > Maintaining safe limits for station and vehicle (i.e. preventing over-filling) while optimizing fill (i.e. reducing under-filling) presents significant challenges
- > Utilizing “target” stop pressure estimates without accounting for additional factors will not meet goals of safety and customer satisfaction

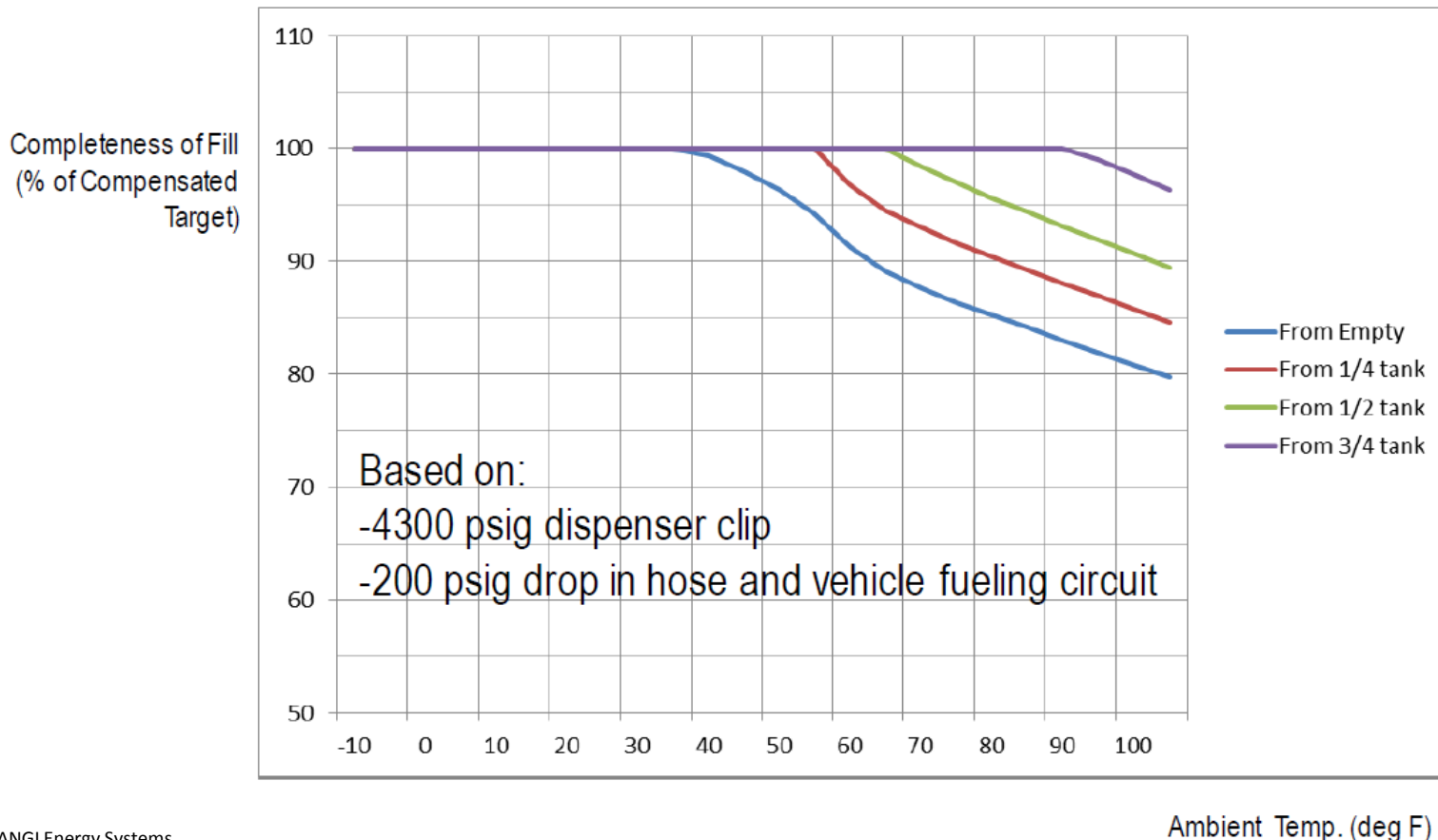
Barrier: Target Stopping Pressure

Target (End of Fill) Tank Pressures



Barrier: Target Stopping Pressure

Fill Completeness Forecast



Achieving a Full-Fill

- > NGV4.3 provides **settled pressure** guideline, **BUT**
- > Dispenser control systems determine end-of-fill stopping **target pressure** (typically elevated pressure based on ambient temp and estimated settling)
- > Under many conditions fills do not reach “full” density
 - Sometimes 20% - 30% less than optimal
- > Driver’s perception of “full” is important
 - Pressure is a poor indication of “full”
 - Temperature compensated fuel gauge

Defining a Full-Fill

- > Full-fill: 3600 psi (settled P) at 70 °F (settled T)
- > Temperature compensation: Correcting for pressure changes due to temp changes in the gas stored
 - “Full” Density: 1800 psi at -40°F and 4500 psi at 130°F
- > Heat of compression: Pressure rise causes temp in cylinder to rise quickly (makes fast-filling difficult)
 - Temporarily high T and P causes fueling procedure to stop with less than “full” density

Defining the Issues

- > High ambient temperatures and amount of gas in cylinder are major contributors to under-filling
 - Though many other factors influence final density
- > Industry direction is demanding better solutions
 - Cylinders are larger (>150 GGEs on-board)
 - Fills are getting faster (high flow dispensers)
 - Success of industry leads to higher expectations (OEMs and very large fleets) and higher impacts for safety/reliability/consistency
- > Safe fills are essential to industry growth

Full-Fills: System Design Parameters

- > Safe operation demands code compliance (ANSI NGV2, NFPA 52, others)
- > Major design parameters include:
 - Max. settled pressure of 3600 psi at 70 °F
 - Max. over-pressurization limit 125% = 4500 psi
 - Max. temperature of cylinder during fill = 180 F
 - Max. pressure relief in dispenser = 4500 psi (4300 psi, practically)
- > Practical operations of station reduce available gas supply

Station Control Improvements

- > Several “solutions” do exist to improve fueling performance
- > Start with dispenser controls/algorithms and then consider other strategies
- > CEC funded GTI under PON-14-502 – Infrastructure Improvement Research for Natural Gas Fueling Stations
- > Major project partner: ANGI Cost Share: SoCalGas
- > Builds on past experience and successes
 - Accufill mass-based fueling protocol



GTI's Current CEC Project

- > The goals of the project are:
 - Develop an advanced fueling control method (including initial characterization step)
 - Design a test system that delivers improved fills
 - Validate and quantify benefits
 - Demonstrate improvements in cost-effectiveness and efficiency of fueling infrastructure and vehicle costs
- > Looking at the issues that are in station's control (i.e. non-communications)
 - Largest, most immediate impact for existing industry

GTI's Current CEC Project

- > Concern is that dispenser pressure tables alone are trying to solve a complex problem with a simple solution – lead to unacceptable under-filling
- > Calculation of internal energy based on variety of variables (known, calculated, and bounded)
- > Accurate control requires compensation for:
 - Initial cylinder gas pressure, temperature, composition
 - Initial station gas pressure, temperature, composition
 - Cylinder volume and thermal resistance (varies by type)
 - Flow rate of gas
 - Ambient Temperature

GTI's Current CEC Project

- > Initial modeling has shown important parameters and consistent results with past testing
 - Simulink modeling to calculate internal energy in cylinder
- > Limited initial testing of baseline dispensers has shown that 20% under-filling occurs
- > Test data from large fleet has shown significant under-filling even when using customer controlled fill settings
- > Design of Experiments: evaluate all variables and quantify their importance
- > Continued modeling and testing over the next year

Potential “Solutions” (or at least advancements)

- > Controls/Algorithm improvements
 - Additional input/data/testing will be needed
 - Potentially leads to standardized control process
- > Station equipment improvements – compressor, valve panels, dispensers
 - Improve hydraulic losses/pressure drops and improve flow, redundant pressure transducers to decrease error
- > Increase pressure limit on dispenser PRDs
 - PRD setting at ~5000 psi would allow stations to utilize existing gas pressure

Potential “Solutions” (or at least advancements)

- > Pre-cooling (i.e. heat exchanger/chiller to lower temperature of supply gas)
 - Done in some situations today; tied to optimized algorithm
 - Disadvantages include capital and operating costs
- > Communications (active or passive)
 - Cylinder volume, cylinder type, gas temperature, gas pressure from vehicle to dispenser would provide benefit
 - Disadvantages include existing vehicles, timing, etc.
- > Vehicle controlled fueling termination
 - Control valve stops fill based on vehicle pressure and temp
 - Control/liability passes to vehicle

Potential “Solutions” (or at least advancements)

- > Vehicle cylinder type can improve heat removal/loss
 - Type IV cylinder is great insulator
 - All other cylinder types have better thermal properties (i.e. provide heat sink and increased conduction)
 - Unclear how effective heat removal is during fast-fill and doesn't lead to industry wide solution
- > Improve “low-end” pressure limits
 - Minimum fuel rail pressure and supply regulator droop = ~200 – 400 psi (5-10% “stranded” gas)
 - Engine/Injector operability limitations
 - Improved equipment on-board vehicle
- > Additional improvements...